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# Low-dispersive Leaky-wave Antenna Integrated in Groove Gap Waveguide Technology

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**Abstract**—In this paper, the use of a dispersive prism with a triangular shape is proposed to reduce the dispersive radiation nature of a leaky-wave antenna in groove gap waveguide technology. The operation of gap waveguide technology is based on the use of metallic pins that act as an artificial magnetic conductor, so the electromagnetic fields are confined and guided in the desired directions. To control a leaky-wave radiation of these confined fields is possible by tailoring the height of the pins, its periodicity and the waveguide width. This radiation, as in any conventional leaky-wave antenna, is dispersive, leading to beam squint as frequency is varied. Here, we mitigate this beam squint by using a prism made of dispersive pins and choosing appropriately their periodicity and height. With this prism, the leaky-wave radiation is focused into one single direction in a wide frequency-band. This concept is demonstrated with a prototype designed to radiate at  $\varphi=41^\circ$  with a central frequency of 12 GHz and high-gain of 16.5 dBi. A 22% frequency bandwidth for the 3-dB realized gain at  $\varphi=41^\circ$  is achieved, and the main radiating direction, with half-power beamwidth of  $5^\circ$ , steers only  $\pm 0.5^\circ$  from 11.4 to 13.4 GHz.

**Index Terms**—Dispersive prism, gap waveguide, leaky-wave antenna.

## I. INTRODUCTION

GAP waveguide is a recent and promising technology for high frequency devices [1]–[3]. Among the advantages of this technology we can point out three. On one hand, the manufacturing is made in two pieces (top and bottom), which simplifies the construction of large and complex devices. Additionally, its losses are low since the propagation is mainly in air, which is only surrounded by a fully-metallic structure in the groove and ridge versions. Finally, no physical contact is needed between the two layers when assembling together, since the electromagnetic band gap (EBG) required in any gap waveguide, inhibits any leakage out of the structure.

Typically, the EBG is constructed with pin-type structures, although other alternatives were proposed in the literatures to reduce their size or cost [4]–[6]. In this paper, we will focus our attention in the classical pin-type configuration. One of the recent challenges in this gap waveguide is to realize efficient

and directive antennas [7], [7]–[9], [9]–[21]. In [7], [7]–[9], [9]–[21], leaky-wave antennas (LWAs) were proposed as an interesting solution due to its structural simplicity and single feeding mechanism. Unfortunately, their principal drawback is that the radiation pattern is dispersive, i.e., the main beam is frequency-scanned [22], thus creating unwanted beam squint which reduces the practical bandwidth with high gain at the desired scanning direction.

The squint effect of leaky-wave antennas is well-known [23]–[28], and many authors have tried to overcome this limitation to keep high gain at the desired scanning direction over a wide band. For example, in [29]–[33], a width-tapering technology is used to improve this characteristic. However, the side effect is a decrease in the directivity or a broaden beam, as discussed in [34]–[36]. Other solutions include the use of coupled-cavity antennas [37], [38], metamaterials [39], metasurfaces [40], anisotropic materials [41], non-reciprocal materials [42], or active non-Foster circuits [43], [44]. All these implementations require of complex structures, multi-layer configurations, expensive materials, or DC biasing that decrease the total efficiency of the system. Also, in [45] a non-dispersive leaky-lens was proposed by immersing a leaky slot line inside a dense dielectric substrate. It is important to note that most of the previous solutions for LWA with reduced beam squint are limited to specific technologies, and they do not present any common solution to reduce the beam squint in general LWAs. For instance, [29], [30], are limited to tapered microstrip LWAs, [31]–[33] can only be implemented in half-width substrate integrated waveguide (SIW) technology, and coupled-SIW technology is required to implement [37], [38]. Similarly [39] is based on metamaterial-based LWAs, the techniques proposed in [41], [42] can only be applied in LWAs with anisotropic or nonreciprocal materials, [43], [44] require active LWAs, and [45] is limited to slot lines leaking power inside a 3D dielectric lens.

In this sense, a novel general technique to reduce the beam squint in any type of LWA was recently proposed in [46]. It is based on the use of a lens which is coupled to the LWA radiation aperture, so that the complementary dispersion of the lens can correct the frequency beam-squint of any dispersive LWA. This technique was demonstrated for the first time in [46] for a LWA in SIW technology, increasing the squint-free bandwidth from 11% to 20%. However, the low-dispersive SIW LWA with a prism proposed in [46] shows a low radiation efficiency of 24% due to the inherent dielectric ohmic losses, resulting in low realized gain of 8.5 dBi in the operating squint-free band.

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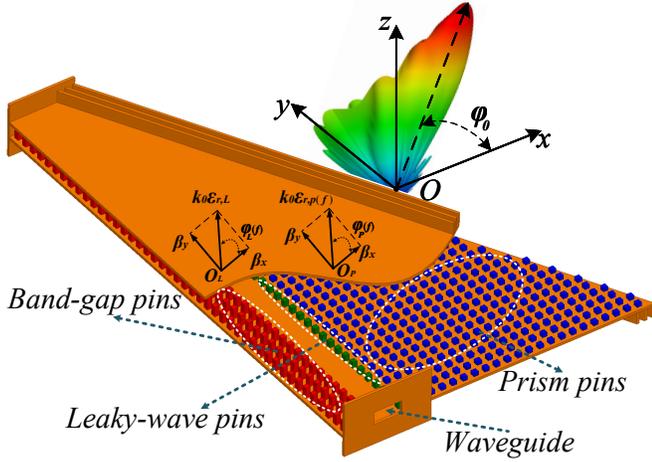


Fig. 1. Non-dispersive leaky-wave antenna in groove gap waveguide technology.

In this paper, we apply this complementary-dispersion prism-coupling technique to reduce the beam squint of a LWA in low-loss groove-gap waveguide technology (GGW), initially proposed in [8]. We demonstrate that the prism-coupling technique can be applied to diverse leaky transmission-line technologies. By choosing GGW technology, lower ohmic losses and higher radiation efficiency than the SIW LWA in [46] are obtained, thus demonstrating for the first time that high-gain and beam-squint reduction are compatible. Moreover, the prism and the GGW LWA are made in the same technology using metallic pins tailored in a common integrated parallel-plate structure, reducing the complexity of the overall device if compared to bulky solutions as the 3D leaky lens in [45]. Our design has a gain of 16.5 dBi with 22% squint-free bandwidth, which is the best performance in terms of gain and squint-free bandwidth for a planar LWA reported so far.

The contents of the paper are as following. Section II presents the dispersion diagram analysis both of the GGW LWA and the dispersive prism, and the design of a proposed antenna is presented in details. Full-wave simulations of the designed antenna are included in Section III whilst the experimental verification constitutes Section IV. A discussion of the designed LWA and a comparative analysis with other reduced-squint LWAs is performed in Section V. Finally the main conclusions of the work are discussed in Section VI.

## II. ANTENNA ANALYSIS AND DESIGN

The configuration of our proposed low-dispersive leaky-wave gap-waveguide antenna is shown in Fig. 1. It consists of two parts, a LWA in GGW technology (created by the red and green pins) and a dispersive metasurface prism (blue pins). The three rows of red pins act as an EBG at the operation frequency, whereas the green row, with pins that are shorter than the red ones, controls the leaky-wave radiation as presented in [8]. Finally, the blue pins, which are the shortest in the structure are aimed to design a dispersive prism which compensates for the dispersion of the leaky wave radiated by

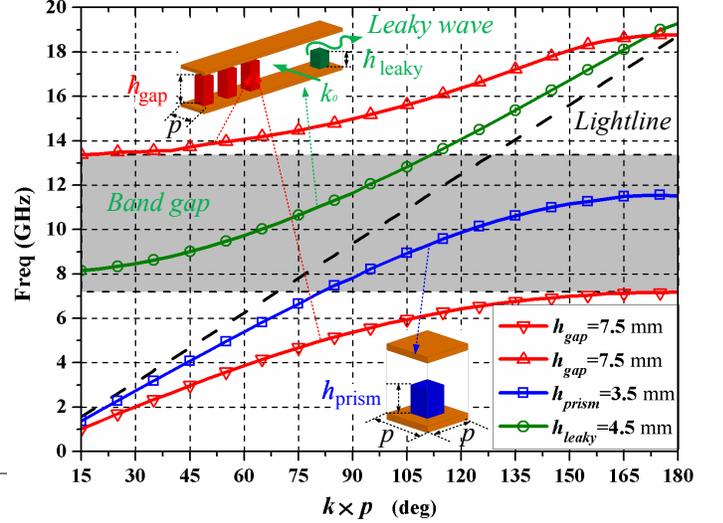


Fig. 2. Dispersion diagram of pins for groove gap waveguide with leaky-wave radiation.

the LWA. The general equations which describe the conditions for dispersion compensation via prism-coupling can be found in [46], and they are not repeated here for the sake of brevity. In the following subsections, this technique is applied for the case of a LWA and a prism integrated in GGW technology as shown in Fig. 1.

### A. Operational Frequency and Dispersion Properties

The first step is to design a groove gap waveguide in X-band by designing the EBG pins (red in Fig. 1). The dispersion characteristic of the metallic pins with a stopband in the X-band is represented in Fig. 2 in red. The red curves show that the red square pins, with a width of 3.5 mm, a height  $h_{gap}$  of 7.5 mm and a periodicity  $p$  of 8.5 mm, have a stopband from 7.2 GHz to 13.4 GHz (grey region). This will be the bandwidth of operation of the groove gap waveguide. In all cases discussed in this paper, the height of the parallel plate structure is considered the height of 10 mm.

As previously demonstrated in [8], a gap waveguide leaky-wave antenna can be designed if one lateral side of a groove structure is replaced by one row made of shorter pins (i.e.,  $h_{leaky}=4.5$  mm) which enables the radiation, as shown in Fig. 2 in green. Its dispersion characteristics are the ones of a conventional  $TE_{10}$ -mode in rectangular waveguides, i.e. a fast wave.

Finally, in the same figure, we represent in blue the dispersion characteristics of periodic metallic pins with a shorter height, ( $h_{prism}=3.5$  mm, blue curve) which is under the light line. This mode has the conventional response of a dispersive dense material, i.e. a slow wave.

It is found that the curve trend of the dispersive prism (blue) is opposite to the one of the leaky-wave gap waveguide (green). Although one is convex and the other is concave, since both have the same trend, it is possible to combine both structures to compensate the overall dispersive behaviour.

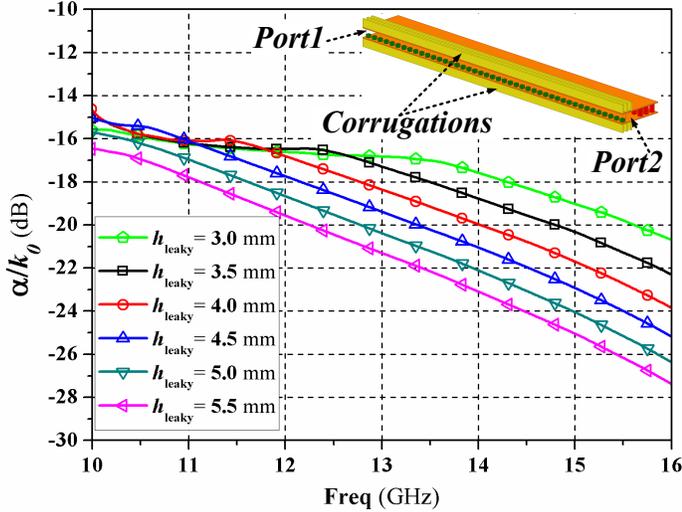


Fig. 3. Amount of radiation of the leaky-wave gap waveguide.

### B. Design of the Leaky-wave Gap Waveguide

After the previous analysis, the design of an antenna with center-frequency at 12 GHz is proposed using the developed methodology in [8]. The designed groove gap-waveguide has a height of 10 mm, a waveguide width of 22 mm and a total length of  $L=374$  mm ( $15\lambda_0$ ).

The selection of the leaky-pin height cannot only be based on the radiation direction (depending on  $\beta_y$ , shown in Fig. 1) of the leaky-wave gap-waveguide, but also a proper leakage constant ( $\alpha$ ) needs to be defined in order to provide optimal radiation and aperture efficiency [22]. The amount of leakage for a number of heights of the pins is represented in Fig. 3 for an aperture length of  $L_R=L \cos(41^\circ)=282.3$  mm. In this study, three corrugated grooves are also added at the aperture of the leaky-wave waveguide as shown in the inset of Fig. 3. These corrugations are employed to reduce the back radiation and hence to increase the gain. This technique was already introduced in [8]. The leakage is calculated as:

$$1 - |S_{11}|^2 - |S_{21}|^2 = 1 - e^{-4\pi \frac{\alpha}{k_0} \frac{L_A}{\lambda_0}} \quad (1)$$

Fig. 3 shows that the leakage with a pin's height of  $h_{leaky}=5.5$  mm is insufficient and this will create low radiation efficiency and therefore poor associated gain. On the other hand, leaky pins with a  $h_{leaky}=3.0$  mm will leak the electromagnetic energy extremely fast, reducing in this case the effective aperture efficiency and leading to poor directivity and gain. Heights of 3.5, 4.0, 4.5 and 5.0 mm are a good compromise for this example.

However, although their  $\alpha$  is appropriate, the radiation direction of this common gap-waveguide leaky-wave antenna presented in [8] will strongly change with the frequency. For example, for  $h_{leaky}=4.5$  mm, the radiation patterns are shown in Fig. 4 from 10.0 to 16.0 GHz. The main-beam angle steers from  $\varphi=45^\circ$  to  $\varphi=65^\circ$ , and the realized peak gain varies from 14 to 19 dBi. As mentioned, this frequency-beam steering strongly reduces the gain bandwidth for a fixed

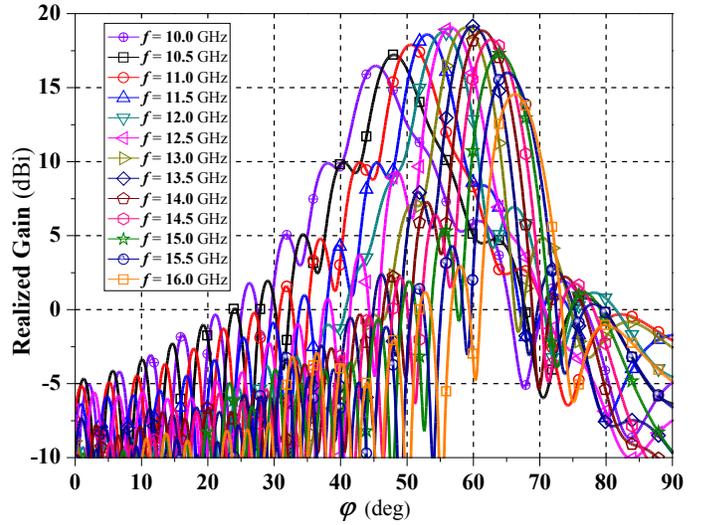


Fig. 4. Beam-steering characteristic of the leaky-wave gap waveguide.

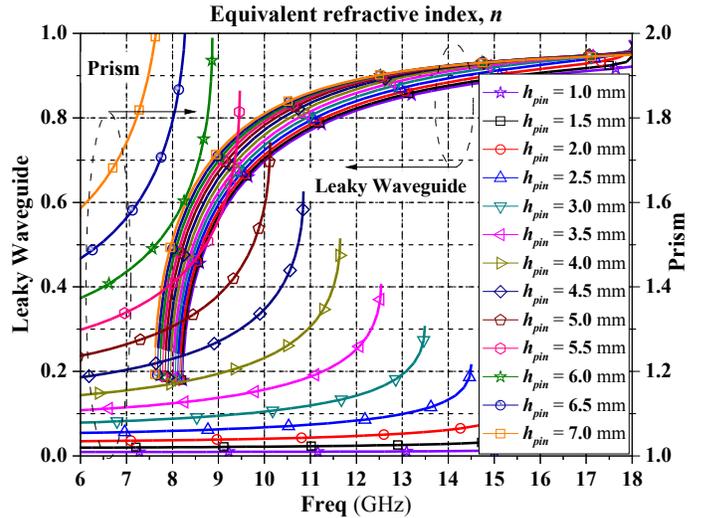


Fig. 5. Equivalent refractive index of periodic pins and the leaky waveguide.

angular direction. This effect is more evident for narrow-beam antennas as the ones needed for high-gain point-to-point wireless links. In our case, the half-power beamwidth is  $6^\circ$  as it corresponds to an aperture length of  $L_R=282.3$  mm at 12 GHz.

### C. Design of Metasurface Prism

Fig. 2 shows two opposite dispersive performance of the GGW LWA and lower-height blue pins, which can be now used to mitigate the squint effect of the designed GGW LWA with the use of a metasurface prism [46]. If we assume that leaky-wave gap waveguide must be designed with  $h_{leaky}$  from 3.5 to 5.0 mm, we must find the appropriate height of the pins of the prism  $h_{prism}$ , to compensate their dispersion.

1) *Equivalent Refractive Index*: From the dispersion diagram in Fig. 2, the equivalent refractive index  $n_P(f)$  of the

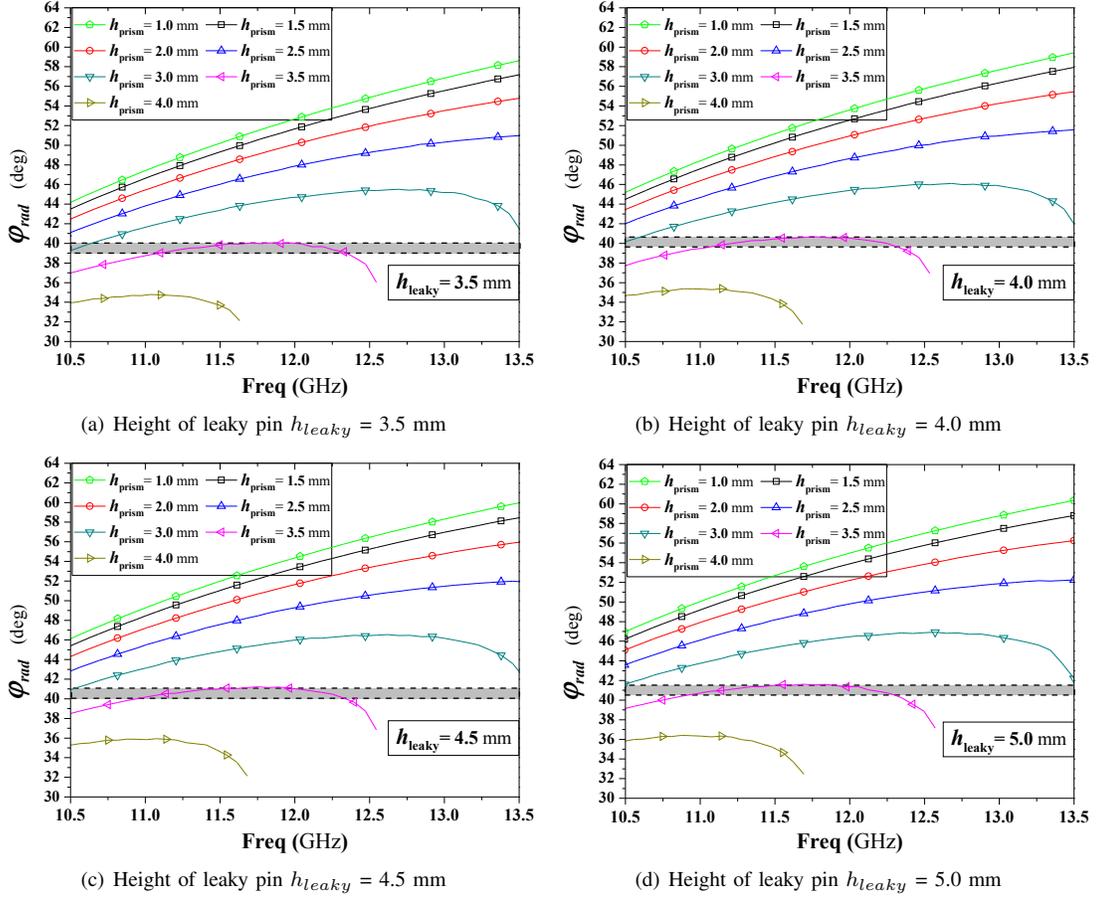


Fig. 6. Calculated radiation direction in the dispersive prism excited with a leaky-wave gap waveguide.

dispersive prism and  $n_L(f)$  of the leaky-wave gap-waveguide can be calculated [46], [47]. Fig. 5 shows both the equivalent refractive indexes of the dispersive prism and the leaky-wave gap-waveguide, for different pin heights,  $h_{pin}$ , varying from 1.0 mm to 7.0 mm. It can be found that the equivalent refractive index of the prism  $n_P(f)$  is concave with frequencies, whereas that of the leaky-wave gap-waveguide  $n_L(f)$  is convex.

2) *Radiation Direction*: Fig. 6 shows the calculated radiation directions ( $\varphi_{rad}$ ) when the height  $h_{prism}$  varies from 1.0 to 4.0 mm for  $h_{leaky}$  varying from 3.5 to 5.0 mm. It can be concluded that with a proper prism design, it is possible to obtain wideband radiation directions. The grey regions in the different figures of Fig. 6 highlight the region where the radiation direction varies only  $\pm 0.5^\circ$  around the center frequency of 12.0 GHz.

#### D. Design of the Complete Antenna

Based on the previous leaky-wave gap waveguide and prism study, a pair of  $h_{leaky}=4.5$  mm and  $h_{prism}=3.5$  mm has been selected for the proposed antenna design. The leaky gap-waveguide aperture lengths is  $L=374$  mm. According to Fig. 6(c), the radiation will be directed at  $\varphi=41^\circ$ . Therefore, the metasurface prism must be cut into a triangle shape with  $41^\circ$  angle and projected length  $L_R$ , to make sure the electromagnetic waves arrive perpendicularly to the radiating

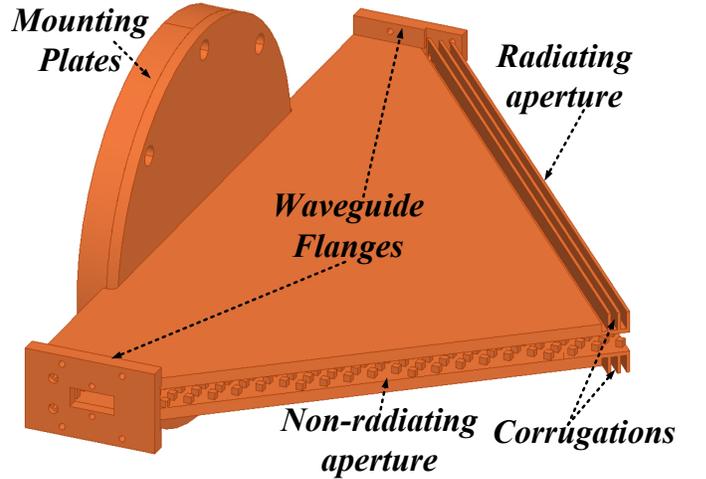


Fig. 7. Complete antenna structure, including flanges, corrugations, and circular plate for the mounting into the anechoic chamber for testing.

aperture. Fig. 7 shows the complete antenna structure, including the two waveguide flanges and three corrugated grooves to improve the radiation efficiency and to reduce the edge diffraction. Moreover, a circular plate is designed to mount the proposed antenna into the rotating platform at the KTH

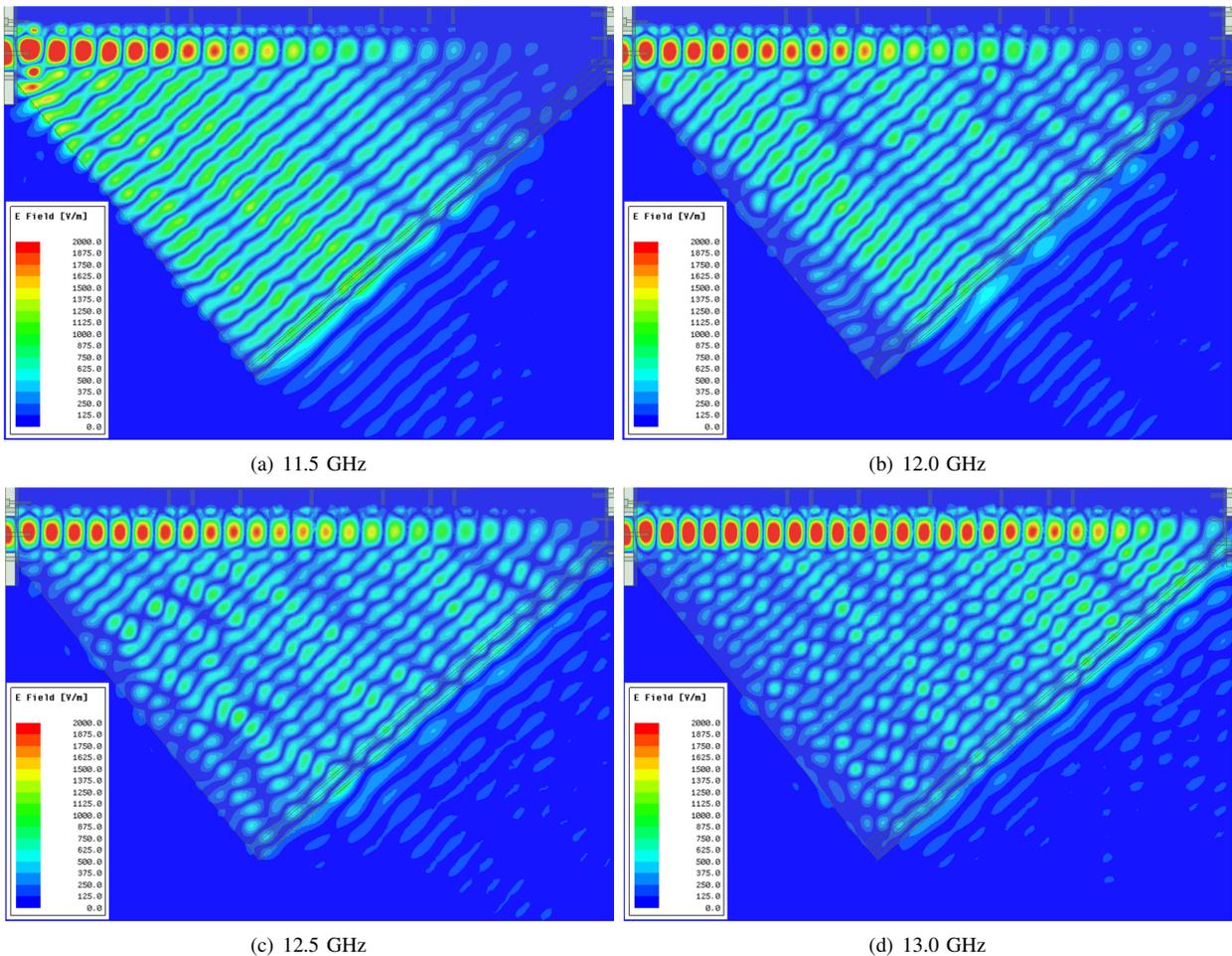


Fig. 8. Amplitude distribution of the electric-field of the proposed antenna.

anechoic chamber. This circular plate has no significant effect in the radiation of the antenna, it is only used for measurement purposes. Finally, in order to reduce the size and weight of the antenna, a cut on the non-radiating side of the prism was made, which is also an improvement from the previous prism in [46].

### III. FULL-WAVE SIMULATION

#### A. Electric-field Distribution

The completed antenna has been modeled and simulated in Ansys HFSS software for validation. The amplitude of the electric-field at four frequencies (11.5, 12, 12.5 and 13 GHz) is represented in Fig. 8. At the four frequencies the electromagnetic waves travel perpendicularly to the radiating aperture. We can also conclude that the leakage  $\alpha$  at low frequencies is stronger than at high frequencies, as is common in leaky-wave antennas [8]. As a result, the aperture efficiency is higher at higher frequencies. On the other hand, at higher frequencies, the amount of radiated fields is lower, so more energy is absorbed by the second port, and the antenna efficiency is decreased. These effects were taken into account and in our design, the total antenna efficiency is higher than 98% from 11.5 to 13.0 GHz.

TABLE I  
RADIATION DIRECTION COMPARISON

Radiation Directions $\varphi$ (deg)					
Leaky-wave Antennas	11.5 GHz	12.0 GHz	12.5 GHz	13.0 GHz	Beam Squinting
Without Prism	53.6	55.7	57.5	59.2	5.6
With Prism	40.6	40.9	41.1	40.5	0.6

#### B. Radiation Patterns

Table. I summarizes the radiation directions including a comparison to the original leaky-wave gap waveguide antenna without the prism. Our proposed leaky-wave antenna has a radiation with a change of only  $0.6^\circ$  in the main radiation direction from 11.5 to 13.0 GHz, whereas the original one has a variation of  $5.6^\circ$ .

Fig. 9 shows the calculated radiation patterns at 11.5, 12.0, 12.5 and 13.0 GHz with realized gain varying from 16.3 to 16.6 dBi. The main-beam half-power width is  $5^\circ$ , as it corresponds to the projected radiating aperture length of the prism (282.3 mm). The main-beam radiation direction remains almost constant at  $\varphi=41^\circ$ . The 3-dB patterns are zoomed to highlight the accuracy of our predictions, as well as to emphasize the obtained 3-dB narrow beamwidth of  $5^\circ$ .

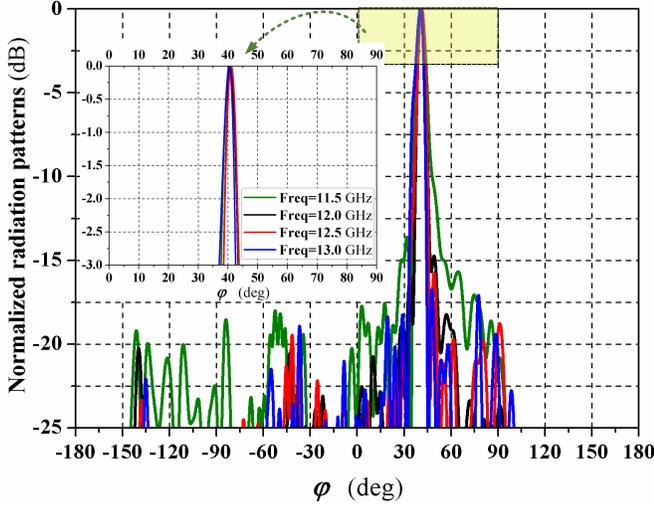


Fig. 9. Radiation patterns at different frequencies.

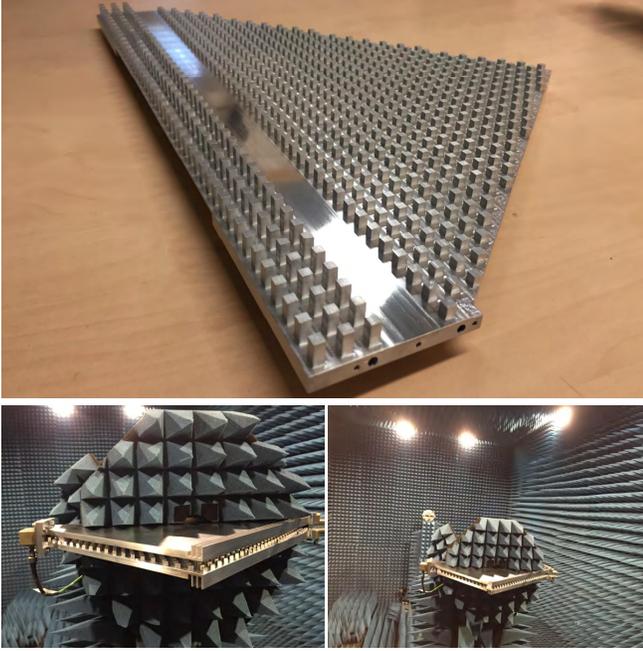


Fig. 10. Prototype of the proposed leaky-wave antenna and measurement setup in the anechoic chamber at KTH.

#### IV. PROTOTYPE AND EXPERIMENTAL RESULTS

A prototype antenna has been manufactured in aluminium as shown in Fig. 10. The prototype was milled in four parts: top cover plate, bottom pins, two feeding waveguide flanges and the circular piece to fix the antenna in the anechoic chamber. These four parts were afterwards assembled together.

##### A. Scattering Parameters

The scattering parameters are shown in Fig. 11. Both simulations and measurements exhibit a good agreement, especially in the  $S_{21}$  parameter. The  $S_{11}$  is below -10 dB from 10.0 to 14.0 GHz, and the  $S_{21}$  is below -15 dB from 10.0 to 13.3 GHz.

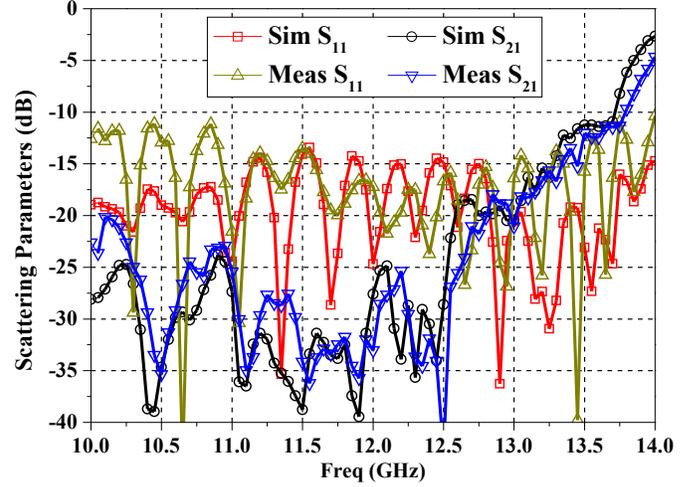


Fig. 11. Scattering parameters of the proposed leaky-wave antenna.

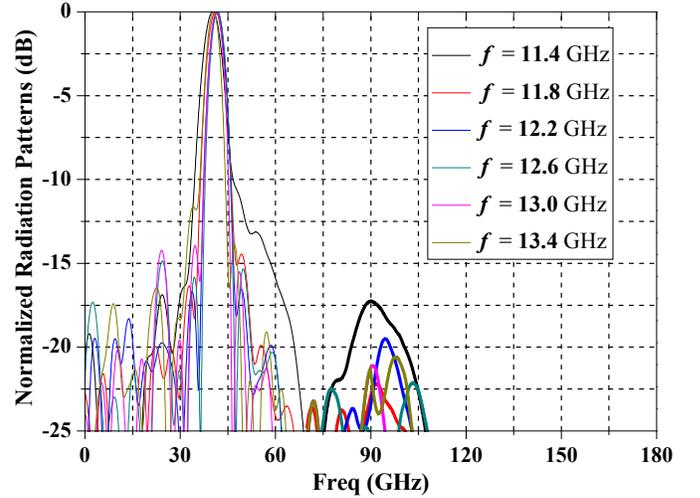


Fig. 12. Measured radiation patterns at different frequencies from 11.4 to 13.4 GHz.

##### B. Radiation Patterns

Fig. 12 shows the measured radiation patterns from 11.4 to 13.4 GHz with a 0.4-GHz step. In all the band, the radiation patterns are directed to  $\varphi=41^\circ$  with  $\pm 0.5^\circ$  difference, which agrees with both the theoretically calculated directions and the full-wave simulations. Moreover, the side-lobe levels (SLL) are all below -13 dB and the half-power beamwidths are around  $5^\circ$ . The peak realized gain at those frequencies also stays very stable, varying from 16.1 to 16.5 dBi, whereas the directivity varies from 16.4 to 16.8 dBi.

Fig. 13 describes the antenna performance in terms of the realized gain at a specific radiation direction as a function of the frequency. It can be found that the proposed low-dispersive leaky-wave antenna has a 22% (2.6 GHz) frequency bandwidth for a measured half-power realized gain at  $\varphi=41^\circ$ , whereas a conventional leaky-wave antenna without prism has a 12.5% (1.5 GHz) frequency bandwidth and its main radiation

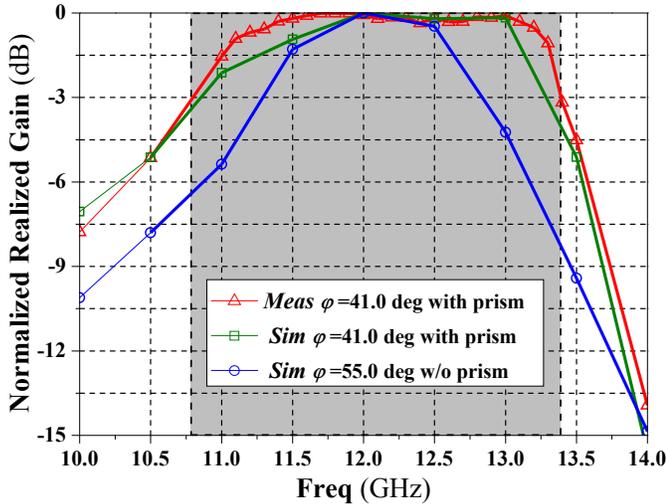


Fig. 13. Normalized realized gain at a specific radiation direction over different frequencies.

direction is  $\varphi=55^\circ$ .

## V. DISCUSSION

The proposed antenna is compared with other published techniques to increase the bandwidth of LWAs [29]-[45]. First, it must be commented that the width-tapering technique applied for microstrip [29]-[30] and SIW [31]-[33] LWAs, produces a strong reduction of the antenna gain. This is due to the associated loss of directivity generated by the broaden of the main beam as explained in [34], [35]. Therefore, this technique is not suitable for high-gain point-to-point directive radio links. Second, most of the solutions proposed in the literature are technology dependent, so that they cannot be applied to any type of LWA whose dispersion wants to be reduced. For instance, the use of coupled cavities proposed in [37]-[38] can only be applied to LWAs based on resonant cavities. In the same manner, the use of metamaterials [39], anisotropic [41], or non-reciprocal [42] materials, can only be applied to LWAs based on such type of artificial materials. Similarly, non-Foster circuits [43], [44] can only be used on LWAs loaded with active circuits, and all these techniques cannot be made extensive to general passive LWAs. Likewise, the LWA lens solution proposed by Neto in [45] can only be applied to a slot-line LWA embedded in a denser medium, and this cannot be extended to other types of LWAs.

On the contrary, the prism-coupling technique used in this paper is independent on the technology of the original LWA (microstrip, SIW, waveguide) whose dispersion has to be reduced. For instance, the authors applied this prism coupling technique to reduce the dispersion of a SIW LWA in [46]. By applying the same technique to a LWA in groove-gap waveguide, we demonstrate its versatility. This versatility is only comparable with the solution proposed in [40] for a coplanar waveguide (CPW) LWA. Therefore, the metasurface solution of [40] and the prism-coupling solution originally proposed in [46], are the only two squint-reduction techniques

that can be applied to general LWAs. For this reason, [40] and [46] are compared with this work in Table II.

First, our solution is much more compact than [40], since the prism can be integrated in a single component together with the original LWA. On the contrary, the metasurface in [40] is coupled to the original LWA via radiation and refraction (as done in transmitarrays), leading to a less compact antenna formed by two distinct parts. This topology can also suffer from reduced efficiency due to diffraction and spillover losses (see Fig.19 in [40]). As summarized in Table II, while the original CPW LWA presented high radiation efficiency of 90%, the addition of the Huygens metasurface strongly reduces the overall antenna efficiency below 50%. On the contrary, the application of the prism-coupling technique to the original dispersive GGW LWA in [8] does not deteriorate its original high-radiation efficiency of 96% as shown in Table II.

Also, our prism loading technique shows better beam squint reduction performance than the use of the Huygens metasurface in [40]. As summarized in Table II, the addition of the prism has demonstrated to reduce the beam squinting to one tenth (from  $5.6^\circ$  to  $0.6^\circ$ ) in a 10% fractional bandwidth (from 11.5 GHz to 13 GHz). This is a stronger mitigation of the beam squinting than the one-half reduction reported in [40] (from  $23.5^\circ$  to  $12^\circ$  in a similar 10% fractional bandwidth). Also, we show in Table II that the Huygens solutions [40] presents lower peak gain of 5 dBi than our design with a high gain of 16.5 dBi, as a result of the reduced efficiency of the overall LWA + metasurface system. Definitely, the prism-coupling technique used in our work shows a much more compact and efficient solution that integrates the LWA and the prism in a single component.

Compared to the SIW LWA with via prism coupling in [46], the proposed gap-waveguide LWA with prism has much higher total antenna efficiency (95% vs. 24%) due to the absence of dielectric ohmic losses. Hence, the proposed LWA has much higher realized antenna gain than [46] (16.5 dBi vs. 8.5 dBi). Even more, the proposed LWA has narrower 3-dB beamwidth ( $5^\circ$  vs.  $9^\circ$ ), and it achieves better beam squinting performance ( $0.6^\circ$  vs.  $1.0^\circ$ ), as summarized in Table II. Moreover, the proposed LWA also has better side-lobe levels (SLLs) (-13 dB vs. -10 dB) and better impedance matching ( $|S_{11}| < -13$  dB vs. -10 dB), and the prism size also gets reduced by cutting the unused prism. Besides, this proposed design is fully metallic thanks to the use of gap waveguide technology instead of SIW. This allows its use for space and for high-power applications.

Furthermore, the LWA design in this paper has an excellent agreement between theoretical, simulated and measured radiation angle ( $\varphi=41^\circ$ ). This is due to the easy implementation of the prism in GGW technology. In the case of the SIW prism, the tight tolerances of design and fabrication of the SIW pins and surrounding slots, create stronger differences between theoretical calculations ( $\varphi=28.5^\circ$ ), full-wave simulations ( $\varphi=24^\circ$ ), and measured radiation angle ( $\varphi=31^\circ$ ) as reported [46]. In conclusion, this work is a better candidate to demonstrate the scenario of loading dispersive prism to LWA in order to reduce the beam squinting or dispersion, not only from the antenna performance, but also from the agreement between theory, full-wave simulation and prototype

TABLE II  
COMPARISON BETWEEN DIFFERENT TECHNIQUES AND TECHNOLOGIES TO REDUCE THE DISPERSION OF GENERAL LWAS

Antenna Type	Frequency Band (GHz)	Beam Angle at Center Frequency (°)	3-dB Beamwidth (°)	Beam Squinting (°)	Peak Gain (dBi)	Antenna Efficiency	SLL (dB)	Integration
CPW LWA [40]	8.4-9.25	15	≈ 16	23.5	4	90%	-4	Two Components (LWA + Metasurface)
CPW LWA + Metasurface [40]	9.5-10.45	14	≈ 14	12	5	< 50%	-6	
GGW LWA [8]	11.5-13.0	55	6	5.6	18	96%	-8	LWA and Prism
SIW LWA + Via Prism [46]	35.0-40.0	31	9	1.0	8.5	24%	-10	Integrated in a Single Component
Gap Waveguide LWA + Pin Prism (this work)	11.5-13.0	41	5	0.6	16.5	95%	-13	

experiment which makes the design more reliable.

## VI. CONCLUSION

We proposed and designed a low-dispersive leaky-wave gap-waveguide antenna, including a theoretical derivation, full-wave simulations and an experimental demonstration. Our proposed methodology is based on the compensation of the dispersion of a leaky-wave radiation with a dispersive metasurface prism, as originally proposed in [46]. Both the antenna and the prism are realized in the same groove-gap waveguide (based on the use of metallic pins on a parallel plate as periodic structure) and its integration as one single component is straightforward.

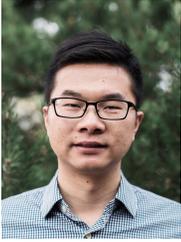
Our proposed leaky-wave antenna has demonstrated to reduce the beam-squint from 6° to 1° in the frequency band of 11.4–13.4 GHz, while maintaining a high directivity of 16.5 dBi with only 5° half-power beamwidth. With the inclusion of a metasurface prism, the frequency bandwidth of the half-power realized gain has been increased from 12.5% to 22%. Although the prism-coupling technique can be applied to other antenna technologies, as demonstrated with a SIW LWA in [46], gap-waveguide technology was selected as a case study due to the reduced ohmic losses. A 95% antenna efficiency in measurement was achieved in our design at the X-band, reporting a much superior performance compared to previous SIW LWA with prism solution [46] in terms of gain due to reduced ohmic losses. Similar superior performance in terms of antenna efficiency is reported when compared to the use of a Huygens metasurface for dispersion-reduction in [40], which suffers from high diffraction losses. To the authors knowledge, the proposed design offers the highest gain and free-squint bandwidth compared to previous squint-free LWAs, and in a compact planar structure, avoiding the use of 3D dielectric lenses as the one proposed in the leaky-lens in [45]. We have also demonstrated that the complementary dispersion prism-coupling technique is not limited to a particular LWA technology, so that it can be applied to low-loss fully-metallic leaky waveguides as the groove-gap guide. These results are very promising for future millimeter-wave point-to-point broadband wireless link applications, where high gain at a given angle must be kept over a wide frequency band. Finally, in terms of contribution to antenna designs with gap waveguide

technology, this contribution is also very relevant as it is the second proposed design in groove gap waveguide technology of a leaky-wave antenna (after [8]). All the advantages of this technology (only metal, contact-less, low loss, easily scalable) are evidenced in this design. It is shown how this technology is probably the most suitable to implement the prism-coupling technique to reduce beam-squinting in leaky-wave antennas.

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